

对数压力坐标系中的公式推导

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由垂直坐标转换的一般关系，得

$$\begin{cases} \frac{d\vec{V}_h}{dt} = -\alpha\nabla_\zeta p - \nabla_\zeta\Phi - f\vec{k} \times \vec{V}_h & (1) \\ \alpha\frac{\partial p}{\partial\zeta} + \frac{\partial\Phi}{\partial\zeta} = 0 & (2) \\ \frac{d}{dt}\left(\ln\frac{\partial p}{\partial\zeta}\right) + \nabla_\zeta \cdot \vec{V}_h + \frac{\partial\dot{\zeta}}{\partial\zeta} = 0 & (3) \\ c_p\frac{dT}{dt} - \alpha\frac{dp}{dt} = \dot{Q} & (4) \end{cases}$$

在对数压力坐标系中，定义

$$z^* \equiv -H\ln\left(\frac{p}{p_s}\right) \quad (5)$$

$$H \equiv \frac{RT_s}{g} \quad (6)$$

令 $\zeta = z^*$ ，则对于(1)，有

$$\frac{d\vec{V}_h}{dt} = -\alpha\nabla_{z^*}p - \nabla_{z^*}\Phi - f\vec{k} \times \vec{V}_h \quad (7)$$

由(5)，得

$$p = \exp\left(\ln p_s - \frac{z^*}{H}\right) \quad (8)$$

因此， p 是 z^* 的函数，故有 $\nabla_{z^*}p = 0$ ，则对于水平运动方程，有

$$\frac{d\vec{V}_h}{dt} = -\nabla_\zeta\Phi - f\vec{k} \times \vec{V}_h \quad (9)$$

$\zeta = z^*$ 对于(2)，有

$$\alpha\frac{\partial p}{\partial z^*} + \frac{\partial\Phi}{\partial z^*} = 0 \quad (10)$$

由(8)，得

$$\frac{\partial p}{\partial z^*} = -\frac{p}{H} \quad (11)$$

又由理想气体的状态方程 $p = \rho RT$, 得

$$\frac{\partial p}{\partial z^*} = -\frac{\rho RT}{H} \quad (12)$$

将上式代入(10), 得到对数压力坐标系下的静力方程

$$\frac{\partial \Phi}{\partial z^*} = \frac{RT}{H} \quad (13)$$

$\zeta = z^*$ 对于(3), 有

$$\frac{d}{dt} \left(\ln \frac{\partial p}{\partial z^*} \right) + \nabla_{z^*} \cdot \vec{V}_h + \frac{\partial z^*}{\partial z^*} = 0 \quad (14)$$

由(11), 得

$$\frac{d}{dt} \left(\ln \frac{\partial p}{\partial z^*} \right) = \frac{d}{dt} \ln \left(-\frac{p}{H} \right) = \frac{d}{dt} (\ln p) = \frac{1}{p} \frac{dp}{dt} \quad (15)$$

令

$$\rho_0(z^*) \equiv \rho_s \exp \left(-\frac{z^*}{H} \right) \quad (16)$$

则

$$\frac{\partial \rho}{\partial z^*} = -\frac{\rho_0}{H} \quad (17)$$

故

$$\frac{w^* \partial \rho_0}{\rho_0 \partial z^*} = -\frac{w^*}{H} \quad (18)$$

又

$$w^* = \frac{dz^*}{dt} = \frac{d}{dt} \left(-H \ln \frac{p}{p_s} \right) = -H \frac{d}{dt} (\ln p - \ln p_s) = -\frac{H}{p} \frac{dp}{dt} \quad (19)$$

所以

$$\frac{w^* \partial \rho_0}{\rho_0 \partial z^*} = \frac{1}{p} \frac{dp}{dt} = \frac{d}{dt} \left(\ln \frac{\partial p}{\partial z^*} \right) \quad (20)$$

又由于

$$\nabla_{z^*} \cdot \vec{V}_h = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \quad (21)$$

$$\frac{\partial z^*}{\partial z^*} = \frac{\partial w^*}{\partial z^*} \quad (22)$$

故(14)变为

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{1}{\rho_0} \frac{\partial(\rho_0 w^*)}{\partial z^*} = 0 \quad (23)$$

由(4), 有

$$c_p \left(\frac{\partial}{\partial t} + \vec{V}_h \cdot \nabla \right) T + c_p w \frac{\partial T}{\partial z} - \alpha \frac{dp}{dt} = \dot{Q} \quad (24)$$

两边同乘以 $\frac{R}{Hc_p}$, 并注意到 $w = \frac{dz}{dt} = \frac{dz}{dp} \frac{dp}{dz} \frac{dz}{dt} = -\frac{1}{\rho g} \frac{dp}{dt}$, 得

$$\left(\frac{\partial}{\partial t} + \vec{V}_h \cdot \nabla \right) \frac{RT}{H} - \frac{R}{\rho g H} \frac{dp}{dt} \frac{\partial T}{\partial z} - \frac{R}{H\rho c_p} \frac{dp}{dt} = \frac{R}{Hc_p} \dot{Q} \quad (25)$$

令 $\kappa = \frac{R}{c_p}$, 并由(13), 上式可变为

$$\left(\frac{\partial}{\partial t} + \vec{V}_h \cdot \nabla \right) \frac{\Phi}{z^*} - \frac{1}{\rho} \frac{dp}{dt} \left(\frac{R}{gH} \frac{\partial T}{\partial z} + \frac{R}{Hc_p} \right) = \frac{\kappa}{H} \dot{Q} \quad (26)$$

又由(6), (19)和理想气体状态方程,

$$-\frac{1}{\rho} \frac{dp}{dt} = -\frac{RT}{p} \frac{T_s}{T_s} \frac{g}{g} \frac{dp}{dt} = -\frac{HgT}{pT_s} \frac{dp}{dt} = w^* \frac{gT}{T_s} \quad (27)$$

则(26)变为

$$\left(\frac{\partial}{\partial t} + \vec{V}_h \cdot \nabla \right) \frac{\Phi}{z^*} + w^* \frac{gT}{T_s} \left(\frac{R}{gH} \frac{\partial T}{\partial z} + \frac{R}{Hc_p} \right) = \frac{\kappa}{H} \dot{Q} \quad (28)$$

由(6), 上式中

$$\frac{gT}{T_s} \left(\frac{R}{gH} \frac{\partial T}{\partial z} + \frac{R}{Hc_p} \right) = \frac{gT}{T_s} \left(\frac{1}{T_s} \frac{\partial T}{\partial z} + \frac{g}{T_s c_p} \right) = \frac{gT}{T_s^2} \frac{\partial T}{\partial z} + \frac{T}{T_s^2} \frac{g^2}{c_p} \quad (29)$$

由于

$$\frac{\partial T}{\partial z} = \frac{\partial T}{\partial z^*} \frac{\partial z^*}{\partial z} = \frac{\partial T}{\partial z^*} \frac{\partial z^*}{\partial p} \frac{\partial p}{\partial z} = \frac{\partial T}{\partial z^*} \frac{H\rho g}{p} = \frac{\partial T}{\partial z^*} \frac{Hg}{RT} = \frac{T_s}{T} \frac{\partial T}{\partial z^*} \quad (30)$$

故

$$\begin{aligned} \frac{gT}{T_s} \left(\frac{R}{gH} \frac{\partial T}{\partial z} + \frac{R}{Hc_p} \right) &= \frac{g}{T_s} \frac{\partial T}{\partial z^*} + \frac{T}{T_s^2} \frac{g^2}{c_p} \\ &= \frac{g}{T_s} \left(\frac{\partial T}{\partial z^*} + \frac{T}{T_s} \frac{g}{c_p} \right) \\ &= \frac{R}{H} \left(\frac{\partial T}{\partial z^*} + \frac{R}{H} \frac{T}{c_p} \right) \end{aligned} \quad (31)$$

由于

$$\theta = T \left(\frac{p_s}{p} \right)^{\frac{R}{c_p}} \quad (32)$$

则

$$\begin{aligned} \frac{\partial \ln \theta}{\partial z^*} &= \frac{\partial}{\partial z^*} \left[\ln T + \frac{R}{c_p} (\ln p_s - \ln p) \right] \\ &= \frac{1}{T} \frac{\partial T}{\partial z^*} - \frac{R}{c_p} \frac{\partial \ln p}{\partial z^*} \\ &= \frac{1}{T} \frac{\partial T}{\partial z^*} + \frac{R}{H c_p} \end{aligned} \quad (33)$$

因此

$$\frac{gT}{T_s} \left(\frac{R}{gH} \frac{\partial T}{\partial z} + \frac{R}{H c_p} \right) = \frac{RT}{H} \frac{\partial \ln \theta}{\partial z^*} \quad (34)$$

令静力稳定度参数

$$S = T \frac{\partial \ln \theta}{\partial z^*} \quad (35)$$

以及

$$N^2 = \frac{R}{H} S \quad (36)$$

则(28)变为

$$\left(\frac{\partial}{\partial t} + \vec{V}_h \cdot \nabla \right) \frac{\Phi}{z^*} + w^* N^2 = \frac{\kappa}{H} \dot{Q} \quad (37)$$

综上, 在对数压力坐标系中, 基本方程组为

$$\left\{ \begin{aligned} \frac{d\vec{V}_h}{dt} &= -\nabla_{\zeta} \Phi - f\vec{k} \times \vec{V}_h \end{aligned} \right. \quad (38)$$

$$\left\{ \begin{aligned} \frac{\partial \Phi}{\partial z^*} &= \frac{RT}{H} \end{aligned} \right. \quad (39)$$

$$\left\{ \begin{aligned} \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{1}{\rho_0} \frac{\partial (\rho_0 w^*)}{\partial z^*} &= 0 \end{aligned} \right. \quad (40)$$

$$\left\{ \begin{aligned} \left(\frac{\partial}{\partial t} + \vec{V}_h \cdot \nabla \right) \frac{\Phi}{z^*} + w^* N^2 &= \frac{\kappa}{H} \dot{Q} \end{aligned} \right. \quad (41)$$